

Machine Design Course for Communication / Electrical Department
Sheet 4 – Shaft Design

Problem 1

Figure 1 is a schematic drawing of a countershaft that supports two belt pulleys. For each pulley, the belt tensions are parallel and for pulley A, the belt tensions are inclined with angle 45° and pulley A consider the loose belt tension is 15 percent of the tension on the tight side. The allowable shear stress of the shaft is 420 MPa. Determine the minimum preferred size diameter. Use the ASME equation when $K_b = 1.5$ and $K_t = 1$.

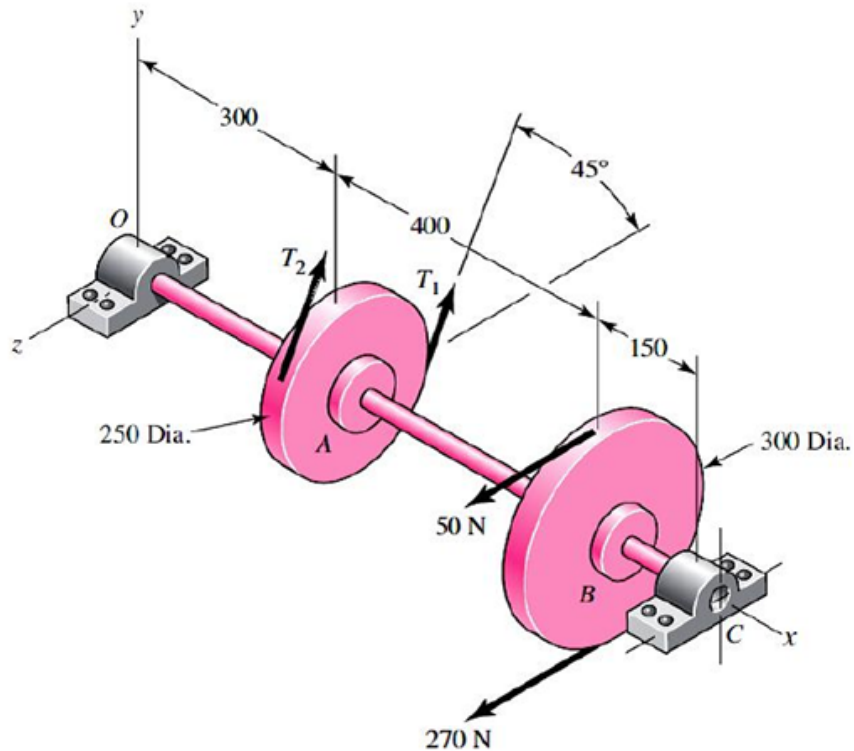


Figure 1.

Givens:

$$\tau_{all} = 420 \text{ Mpa}$$

$$K_b = 1.5 \text{ and } K_t = 1 \quad T_2 = 0.15T_1$$

Req: $d = ?$

Solution

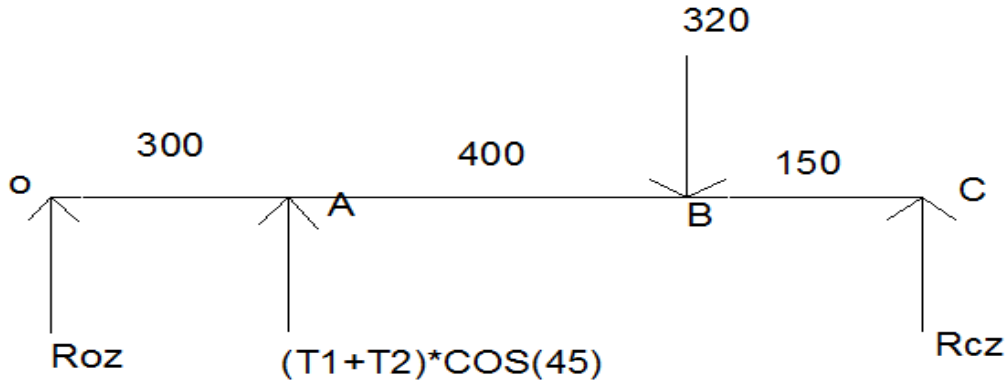
Max torque calculation:

$$T_A = T_B$$

$$(T_1 - T_2) * \frac{250}{2} = (270 - 50) * \frac{300}{2}$$

$$(T_1 - 0.15T_1) * \frac{250}{2} = (270 - 50) * \frac{300}{2}$$

$T_1=310.588 \text{ N}$ $T_2=46.5882 \text{ N}$
 X-Z plane



$\sum M_0=0$

$(T_1+T_2)*\text{COS}(45)*300-320*(300+400)+R_{cz}*(300+400+150)=0$

$R_{cz}=174.3899 \text{ N}$

$\sum T_z=0$

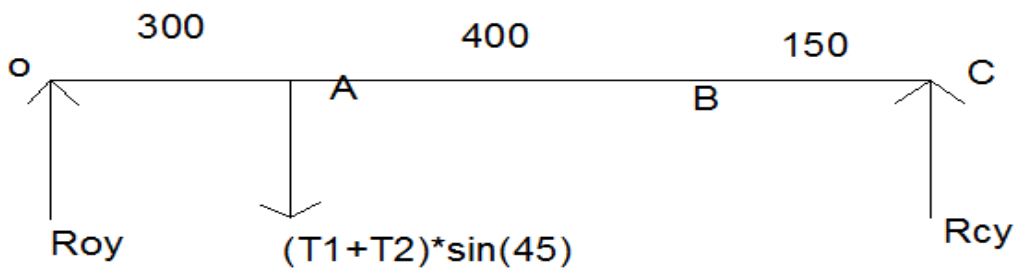
$R_{oz}+(T_1+T_2)*\text{COS}(45)-320+R_{cz}=0$

$R_{oz}=-106.95 \text{ N}$

$M_{az}= R_{oz}*300=-32079 \text{ N.mm}$

$M_{bz}= R_{cz}*150=26158.48 \text{ N.mm}$

X-Y plane



$\sum M_0=0$

$(T_1+T_2)*\text{sin}(45)*300+R_{cy}*(300+400+150)=0-$

$R_{cy}=89.139 \text{ N}$

$\sum F_y=0$

$R_{oy}-(T_1+T_2)*\text{sin}(45)+R_{cy}=0$

$R_{oy}=163.4227 \text{ N}$

$M_{ay}= R_{oy}*300=49026.8 \text{ N.mm}$

$M_{by}= R_{cy}*150=13370.85 \text{ N.mm}$

so:

$M_a=\sqrt{M_{az}^2 + M_{ay}^2}$

$$=49131.71 \text{ N.mm}$$

$$M_b = \sqrt{M_{bz}^2 + M_{by}^2}$$

$$=29377.64 \text{ N.mm}$$

$$T_a = T_b = (270 - 50) * 300 / 2 = 33000 \text{ N.mm}$$

Design based on point (A)

$$d_o = \left[\frac{16}{\pi * 420} * \sqrt{(1.5 * 49131.71)^2 + (33000)^2} \right]^{1/3}$$

$$d_o = 9.93 \approx 10 \text{ mm}$$

Problem 2

A gear-reduction unit uses the countershaft depicted in Figure 2. The allowable shear stress of the shaft is 420 MPa. Determine the minimum preferred size diameter. Use the ASME equation when $K_b = K_t = 1.5$.

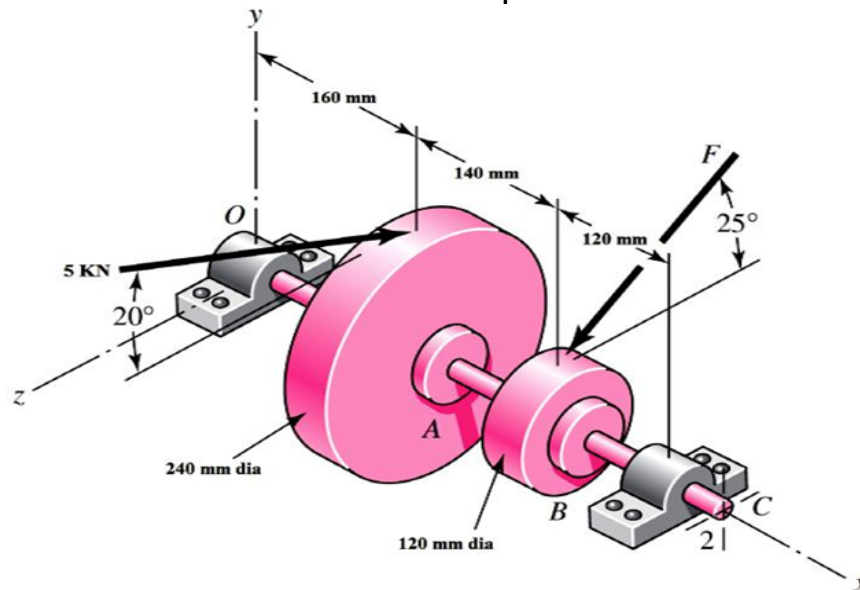


Figure 2.

Givens:

$$\tau_{all} = 420 \text{ Mpa}$$

$$K_b = K_t = 1.5$$

$$\text{Req: } d = ?$$

Solution

Max torque calculation:

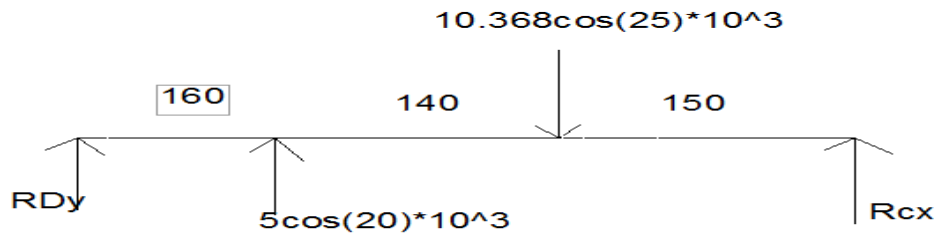
$$T_A = F_A * \cos(20) * \frac{D_A}{2} = 5 * 10^3 * \cos(20) * \frac{240}{2} = 563.815 * 10^3 \text{ N.mm}$$

$$T_A = T_B$$

$$F_B \cdot \cos(25) \cdot \frac{120}{2} = 563.815 \cdot 10^3$$

$$F_B = 10.36835 \text{ N}$$

Max moment calculations:



$$\sum M_0 = 0$$

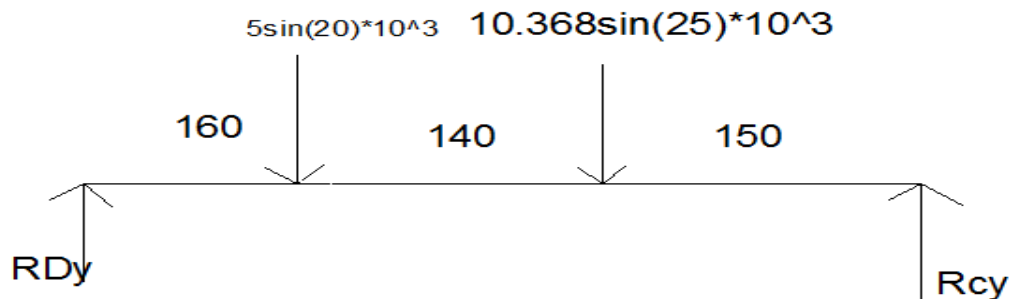
$$5 \cdot \cos(20) \cdot 10^3 \cdot 160 - 10.368 \cdot \cos(25) \cdot 10^3 \cdot (160 + 140) + R_{cx} \cdot (160 + 140 + 150) = 0$$

$$R_{cx} = 4.5938 \cdot 10^3 \text{ N}$$

$$R_{Ox} = 0.104336 \cdot 10^3 \text{ N}$$

$$\text{Max} = R_{Ox} \cdot 160 = 0.104336 \cdot 10^3 \cdot 160 = 16.697376 \cdot 10^3 \text{ N.mm}$$

$$\text{Mbx} = R_{cx} \cdot 150 = 4.5938 \cdot 10^3 \cdot 150 = 689.07 \cdot 10^3 \text{ N.mm}$$



$$\sum M_0 = 0$$

$$-5 \cdot \sin(20) \cdot 10^3 \cdot 160 - 10.368 \cdot \sin(25) \cdot 10^3 \cdot (160 + 140) + R_{cy} \cdot (160 + 140 + 150) = 0$$

$$R_{cy} = 3.529 \cdot 10^3 \text{ N}$$

$$R_{Oy} = 2.5628 \cdot 10^3 \text{ N}$$

$$\text{May} = R_{Oy} \cdot 160 = 2.562 \cdot 10^3 \cdot 160 = 409.92 \cdot 10^3 \text{ N.mm}$$

$$\text{Mby} = R_{cy} \cdot 150 = 3.529 \cdot 10^3 \cdot 150 = 529.35 \cdot 10^3 \text{ N.mm}$$

so:

$$\text{Ma} = \sqrt{\text{Max}^2 + \text{May}^2} = 410.259 \cdot 10^3 \text{ N.mm}$$

$$\text{Mb} = \sqrt{\text{Mbx}^2 + \text{Mby}^2} = 868.92 \cdot 10^3 \text{ N.mm}$$

Design based on point (B)

$$d_o = \left[\frac{16}{\pi \cdot 420} \cdot \sqrt{(1.5 \cdot 868.92 \cdot 10^3)^2 + (1.5 \cdot 563.815 \cdot 10^3)^2} \right]^{1/3}$$

$$d_o = 26.6 \approx 27 \text{ mm}$$

Problem 3

A shaft made of steel receives 7.5 kW power at 1500 r.p.m. A 450 mm diameter pulley mounted on the shaft as shown in Figure 3 has ratio of belt tensions of 4. The allowable shear stress of the shaft is 420 MPa. The gear diameter is 200 mm and $F_r = 0.2 F_t$. Design the shaft diameter. Use the ASME equation when $K_b = 1.5$ and $K_t = 1$.

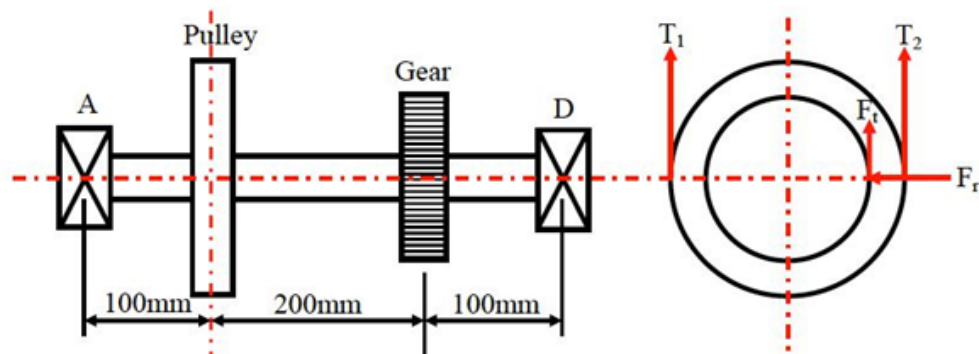


Figure 3.

Givens:

$$P = 7.5 \text{ Kwatt}$$

$$K_b = 1.5 \text{ and } K_t = 1$$

$$N = 1500 \text{ rpm}$$

$$\tau_{\text{all}} = 420 \text{ Mpa}$$

$$F_r = 0.2 F_t$$

$$T_1 = 4 \cdot T_2$$

$$\text{Req: } d = ?$$

Solution

Max torque calculation:

$$P = T \cdot \omega \quad \rightarrow \quad 7.5 \cdot 10^3 = T \cdot (2 \cdot \pi \cdot 1500 / 60)$$

$$T = 47.746 \cdot 10^3 \text{ N.mm}$$

$$T_{\text{pulley}} = (T_1 - T_2) \cdot 450 / 2 \quad \rightarrow \quad 47.746 \cdot 10^3 = (4T_2 - T_2) \cdot 450 / 2$$

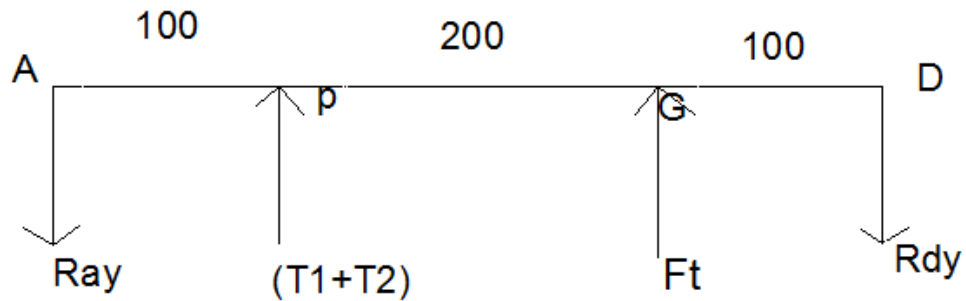
$$T_1 = 4T_2 = 282.93 \text{ N}$$

$$T = T_{\text{bar}} = F_t \cdot 200 / 2 = 47.746 \cdot 10^3$$

$$F_t = 477.46 \text{ N}$$

$$F_r = 0.2 F_t = 95.492 \text{ N}$$

y-z plane



$$\sum M_{Ax}=0$$

$$(T1+T2*100+Ft*(100+200)-Rdy*(100+200+100))=0$$

$$Rdy=446.511 \text{ N}$$

$$\sum Fy=0$$

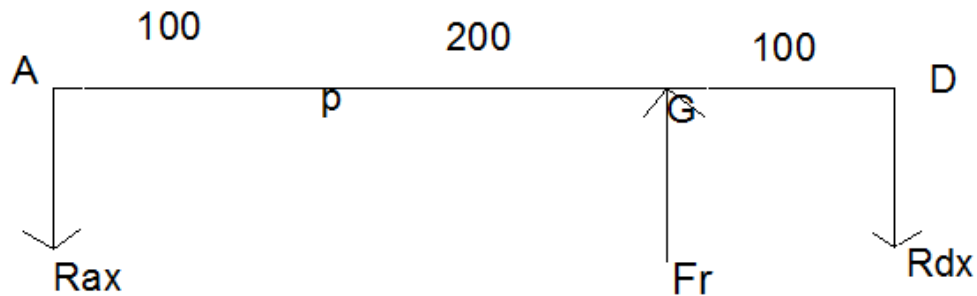
$$Ray-(T1+T2-Ft+Rdy)=0$$

$$Ray=384.613 \text{ N}$$

$$Mpy= -Ray*100=-38.46*10^3 \text{ N.mm}$$

$$MGy= -Rdy*100=-44.6511*10^3 \text{ N.mm}$$

X-Z plane



$$\sum M_{Ay}=0$$

$$Fr*(100+200)-Rdx*(100+200+100)=0$$

$$Rdx=71.619 \text{ N}$$

$$\sum Fx=0$$

$$Rax-Fr+Rdx=0$$

$$Rax=23.873 \text{ N}$$

$$Mpx= -Rax*100=-2.3873*10^3 \text{ N.mm}$$

$$MGx= -Rdx*100=-7.1619*10^3 \text{ N.mm}$$

G have the maximum moment so:

$$M_G = \sqrt{M_{G,x}^2 + M_{G,y}^2} = 45.2218 \cdot 10^3 \text{ N.mm}$$

$$T_G = 47.746 \cdot 10^3 \text{ N.mm}$$

Design based on point (G)

$$d_o = \left[\frac{16}{\pi \cdot 420} \cdot \sqrt{(1.5 \cdot 45.2218 \cdot 10^3)^2 + (1 \cdot 47.746 \cdot 10^3)^2} \right]^{1/3}$$

$$d_o = 0.5288 \approx 1 \text{ mm}$$

Problem 4

A horizontal shaft AD supported in bearings at A and B and carrying pulleys at C and D is to transmit 75 kW at 500 r.p.m. from drive pulley D to off-take pulley C, as shown in Figure 4. Calculate the diameter of shaft. The data given is: $P_1 = 3 P_2$ (both horizontal), $Q_1 = 2 Q_2$ (both vertical), radius of pulley C is 220 mm, radius of pulley D is 160 mm, The allowable shear stress of the shaft is 420 MPa. Use the ASME equation when $K_b = 1.5$ and $K_t = 1$.

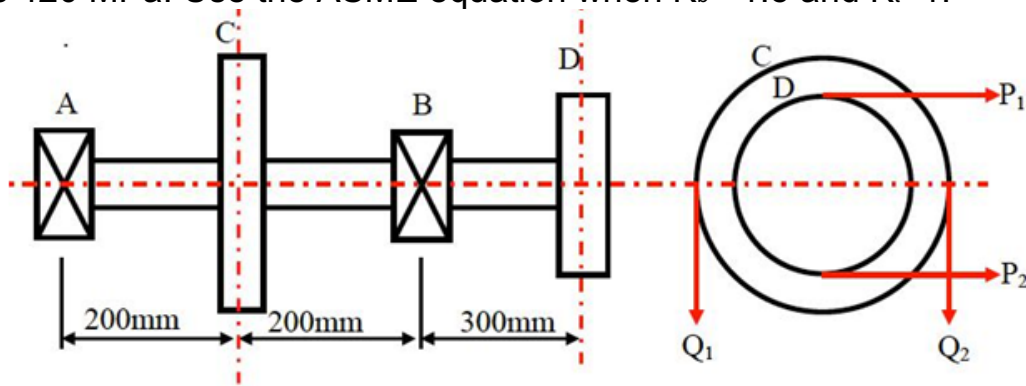


Figure 4.

Givens:

$$P = 75 \text{ Kwatt}$$

$$K_b = 1.5 \text{ and } K_t = 1$$

$$N = 500 \text{ rpm}$$

$$\tau_{all} = 420 \text{ Mpa}$$

$$\text{Req: } d = ?$$

Solution

Max torque calculation:

$$P = T \cdot \omega \rightarrow 75 \cdot 10^3 = T \cdot (2 \cdot \pi \cdot 500 / 60)$$

$$T = 1.43239 \cdot 10^6 \text{ N.mm}$$

$$T_D = (P_1 - P_2) * r_D$$

$$1.43239 * 10^6 = (3P_2 - P_2) * 160$$

$$P_2 = 4.4762 * 10^3 \text{ N}$$

$$P_1 = 13.4286 * 10^3 \text{ N}$$

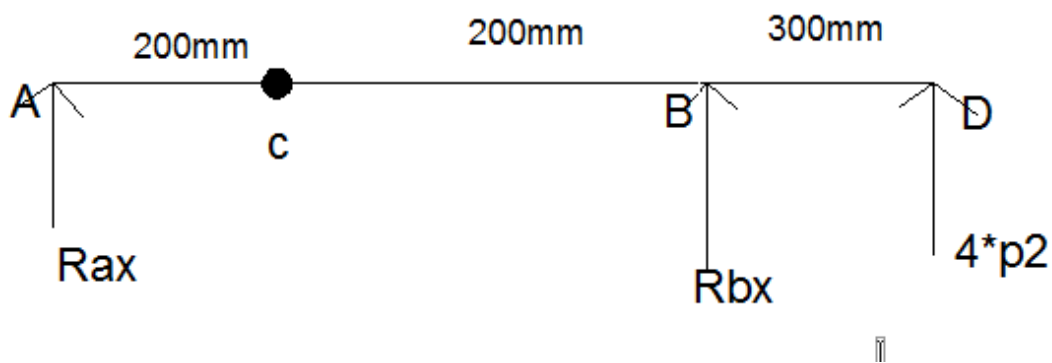
$$T_A = (Q_1 - Q_2) * r_C$$

$$1.43239 * 10^6 = (2Q_2 - Q_2) * 220$$

$$Q_2 = 6.51086 * 10^3 \text{ N}$$

$$Q_1 = 13.0217 * 10^3 \text{ N}$$

Max moment calculations:



$$\sum M_{max} = 0$$

$$R_{bx} * (200 + 200) - 4 * (4.4762 * 10^3) * (200 + 200 + 300) = 0$$

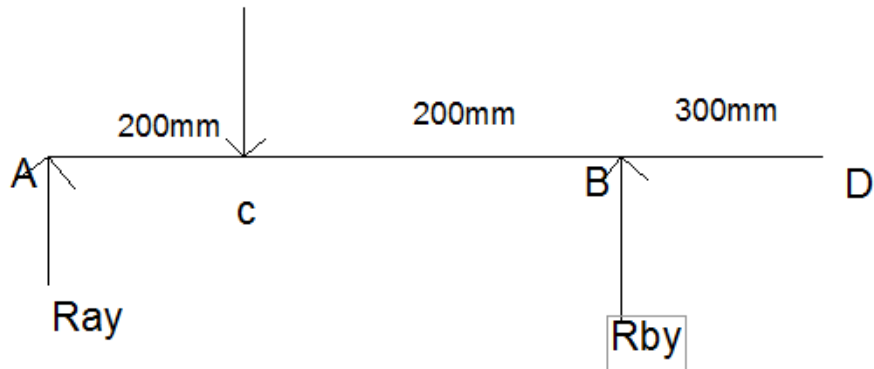
$$R_{bx} = 31.3334 * 10^3 \text{ N}$$

$$R_{ax} + R_{bx} = 4 * p_2$$

$$R_{ax} = 4 * 4.4762 * 10^3 - 31.3334 * 10^3 = -13.4292 * 10^3 \text{ N}$$

$$M_{cx} = R_{ax} * 200 = -13.4292 * 10^3 * 200 = -2.68584 * 10^6 \text{ N.mm}$$

$$M_{bx} = 4 * p_2 * 300 = 5.37144 * 10^6 \text{ N.mm}$$



$$\sum M_A = 0$$

$$R_{by} \cdot (200 + 200) - 3 \cdot (6.5108 \cdot 10^3) \cdot (200) = 0$$

$$R_{by} = 9.7662 \cdot 10^3 \text{ N}$$

$$R_{ay} + R_{by} = 3 \cdot Q_2$$

$$R_{ay} = 3 \cdot 6.5108 \cdot 10^3 - 9.7662 \cdot 10^3 = 9.7662 \cdot 10^3 \text{ N}$$

$$M_{cy} = R_{ay} \cdot 200 = 9.7662 \cdot 10^3 \cdot 200 = 1.95324 \cdot 10^6 \text{ N}\cdot\text{mm}$$

$$M_{by} = 0 \text{ N}\cdot\text{mm}$$

so:

$$M_c = \sqrt{M_{cx}^2 + M_{cy}^2} = 3.3209 \cdot 10^6 \text{ N}\cdot\text{mm}$$

$$M_b = \sqrt{M_{bx}^2 + M_{by}^2} = 5.37144 \cdot 10^6 \text{ N}\cdot\text{mm}$$

Design based on point (B)

$$d_o = \left[\frac{16}{\pi \cdot 45} \cdot \sqrt{(1.5 \cdot 5.37144 \cdot 10^6)^2 + (1 \cdot 1.43239 \cdot 10^6)^2} \right]^{1/3}$$

$$d_o = 97.47 \approx 98 \text{ mm}$$